

IIR Filter Designing Using Butterworth Approximation

1 What is Butterworth Approximation?

1. Butterworth lowpass filter (LPF) was proposed by Butterworth in 1930 in his paper titled: *On the Theory of Filter Amplifiers* (Link: https://www.changpuak.ch/electronics/downloads/On_the_Theory_of_Filter_Amplifiers.pdf).

2. He proposed that, any filter with its frequency response $H(\Omega)$ that satisfies the equation

$$|H(\Omega)|^2 = \frac{1}{1 + \left(\frac{\Omega}{\Omega_c}\right)^{2N}} \quad (1)$$

is a low pass filter with order N and cutoff frequency Ω_c .

3. The Laplace transform $H(s)$ follows the equation,

$$H(s)H(-s) = \frac{1}{1 + \left(\frac{s}{j\Omega_c}\right)^{2N}} \quad (2)$$

4. The roots of (2) are given by,

$$s_k = \Omega_c e^{j\frac{\pi}{2} \frac{2k+1+N}{N}} \quad (3)$$

where, $k = \{0, 1, 2, \dots, 2N - 1\}$.

5. We consider the roots that lie in the left hand side of the $j\Omega$ axis which are obtained by varying k from 0 to $N - 1$.

6. Therefore, the Butterworth low pass filter is given as,

$$H(s) = \frac{1}{\prod_{k=0}^{N-1} (s - s_k)} \quad (4)$$

where, s_k is given by (3).

2 Bilinear Transform

The Butterworth approximation for analog filters can be used for construction digital IIR filters using Bilinear transform. The Bilinear transform establishes a relationship between s (Laplace) and z (Z transform). The mapping, given by *Bilinear Transform*, is given by the equation

$$s = \frac{2}{T} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right) \quad (5)$$

Where, T is the sampling duration. Due to this transformation, a non-linear mapping from Ω to ω is obtained, defined by,

$$\Omega = \frac{2}{T} \tan\left(\frac{\omega}{2}\right) \quad (6)$$

Or,

$$\omega = 2 \tan^{-1}\left(\frac{\Omega T}{2}\right) \quad (7)$$

The above effect is known as *frequency warping*. In order to remove this warping effect, the analog frequencies are *prewarped* using the equation 6.

Point to be noted is that, for simplicity of calculations, we shall consider $T = 2$. Considering this won't cause any harm as the factor $T/2$ would get cancelled while doing Bilinear transformation. Hence the equation (6) to be used for prewarping reduces to,

$$\Omega = \tan\left(\frac{\omega}{2}\right) \quad (8)$$

And equation (7) reduces to,

$$\omega = 2 \tan^{-1} \Omega \quad (9)$$

The normalized denominator polynomials for different order N are as shown in Table 1.

Table 1: Denominator Polynomials for Butterworth Filters with Order N

Order (N)	Denominator Polynomial
1	$s + 1$
2	$s^2 + 1.414s + 1$
3	$(s + 1)(s^2 + s + 1)$
4	$(s^2 + 0.766s + 1)(s^2 + 1.848s + 1)$
5	$(s + 1)(s^2 + 0.618s + 1)(s^2 + 1.618s + 1)$
6	$(s^2 + 0.518s + 1)(s^2 + 1.414s + 1)(s^2 + 1.932s + 1)$
7	$(s + 1)(s^2 + 0.445s + 1)(s^2 + 1.247s + 1)(s^2 + 1.802s + 1)$

3 Designing Digital IIR Low Pass Filter

Example: Design a digital low pass filter with specifications as:

$$-2dB \leq |H(\omega)| \leq 0 \quad = 0 \leq \omega \leq 0.2\pi$$

$$|H(\omega)| \leq -15dB \quad = 0.5\pi \leq \omega$$

- **Step 0: Interpreting the specifications and prewarping the frequencies.**

Following specifications can be observed:

Passband edge: $\omega_p = 0.2\pi$.

Stopband edge: $\omega_s = 0.5\pi$.

Passband attenuation: $A_p = -2dB$.

Stopband attenuation: $A_s = -15dB$.

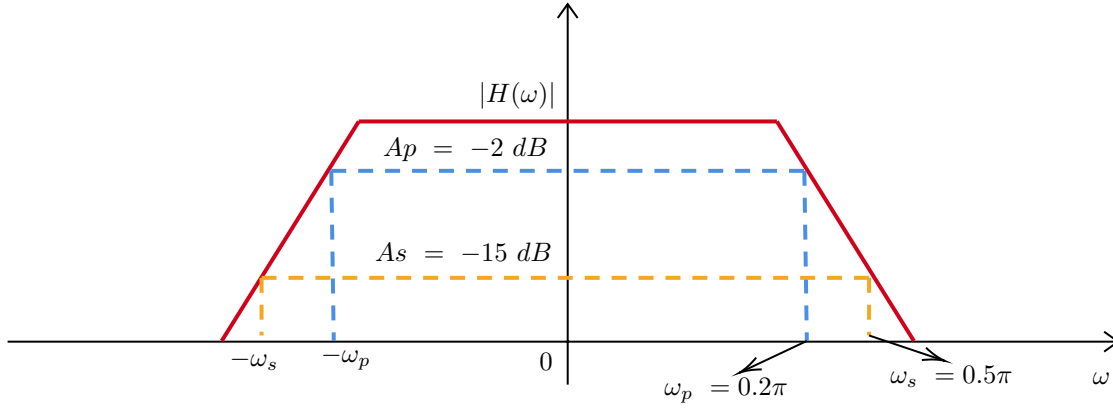


Figure 1: Low Pass Filter Specifications

Prewarping:

$$\Omega_{p,LP} = \tan\left(\frac{\omega_p}{2}\right) = \tan\left(\frac{0.2\pi}{2}\right) = 0.3249$$

$$\Omega_{s,LP} = \tan\left(\frac{\omega_s}{2}\right) = \tan\left(\frac{0.5\pi}{2}\right) = 1$$

- **Step 1: Frequency Mapping For Obtaining Normalized LPF**

Generally, for design of any IIR filter, the pass band edge of prototype LPF is mapped to 1 and corresponding changes that occur are as,

$$\Omega_{mapped} = \frac{\Omega}{\Omega_{p,LP}} \quad (10)$$

So, we have,

$$\begin{aligned} \Omega_p &= 1 \\ \Omega_s &= \frac{\Omega_{s,LP}}{\Omega_{p,LP}} = \frac{1}{0.3249} = 3.0779 \end{aligned}$$

The mapping is as shown in Fig. 2

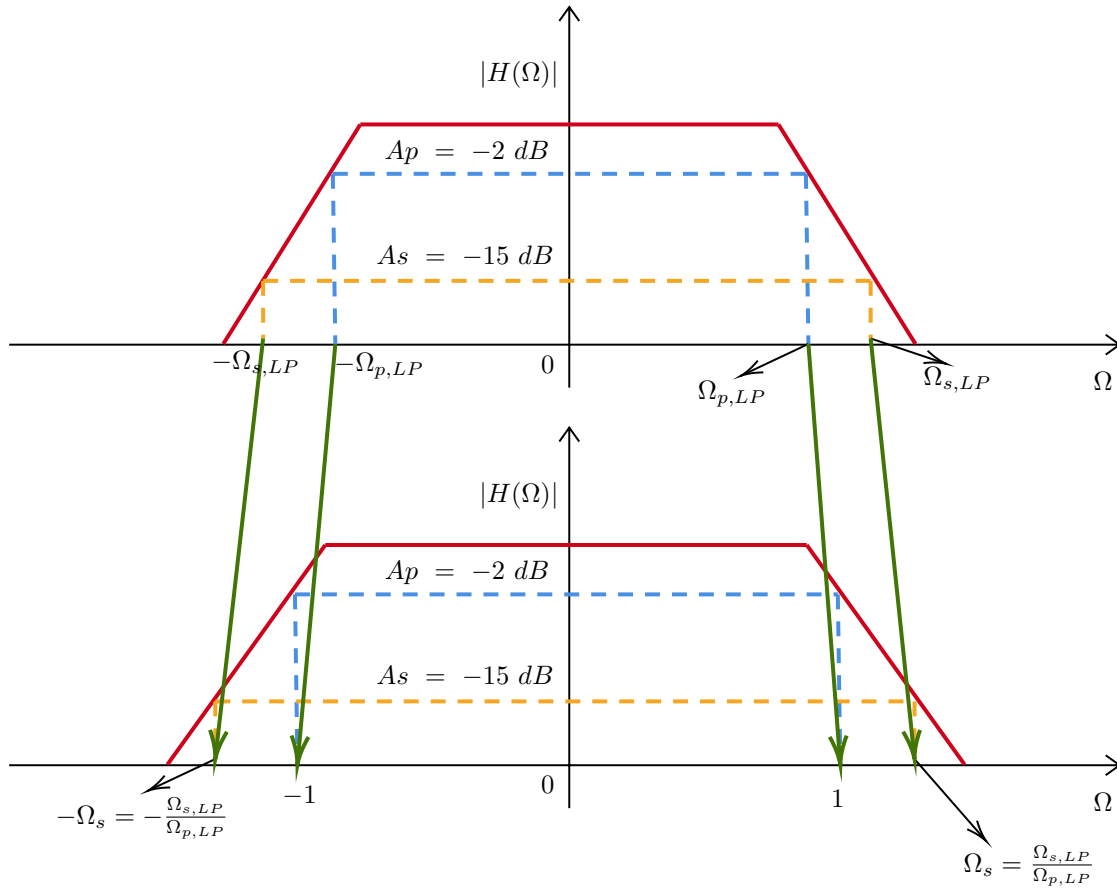


Figure 2: Mapping For Low Pass filter

- **Step 2: Finding Order for the Prototype LPF**

In order to find the LPF, first we need to find the order. The order can be found using the formula:

$$N = \frac{\log\left(\frac{10^{|A_s|/10} - 1}{10^{|A_p|/10} - 1}\right)}{2 \times \log\left(\frac{\Omega_s}{\Omega_p}\right)}$$

For considered example,

$$N = \frac{\log\left(\frac{10^{15/10} - 1}{10^{2/10} - 1}\right)}{2 \times \log\left(\frac{3.0779}{1}\right)} = \lceil 1.76 \rceil = 2.$$

- **Step 3: Find Normalized LPF Equation by Finding roots or Using Polynomial Table**

We have,

$$s_k = e^{j\frac{\pi}{4}(2k+3)} \quad (11)$$

As $N = 2$, $k = \{0, 1\}$. So, we have,

$$s_o = e^{j\frac{3\pi}{4}}$$

and

$$s_1 = e^{j\frac{5\pi}{4}}$$

Using the roots, the value of $H(s)$ can be found as,

$$\begin{aligned} H(s) &= \frac{1}{(s - s_0)(s - s_1)} \\ &= \frac{1}{(s - e^{j\frac{3\pi}{4}})(s - e^{j\frac{5\pi}{4}})} \\ H(s) &= \frac{1}{s^2 + 1.414s + 1} \end{aligned}$$

- **Step 4: Find the cutoff frequency.**

The cutoff frequency of the filter is unknown and can be found as,

$$\Omega_c = \frac{\Omega_s}{(10^{|A_s|/10} - 1)^{\frac{1}{2N}}} \quad (12)$$

For, this example,

$$\Omega_c = \frac{3.0779}{(10^{15/10} - 1)^{\frac{1}{4}}} = 1.3084 \quad (13)$$

- **Step 5: Find Denormalized Cutoff Frequency**

This cutoff frequency is not the actual cutoff frequency but it is frequency when passband edge is mapped to 1. So, the actual cutoff is given by,

$$\Omega_{c,actual} = \Omega_c \times \Omega_{p,LP} = 1.3084 \times 0.3249 = 0.4251 \quad (14)$$

- **Step 6: Find Analog Filter**

In order to find LPF, substitute $s \rightarrow \frac{s}{\Omega_{c,actual}}$.

$$\begin{aligned} H(s)|_{s \rightarrow \frac{s}{\Omega_{c,actual}}} &= \frac{1}{\left(\frac{s}{\Omega_{c,actual}}\right)^2 + 1.414\left(\frac{s}{\Omega_{c,actual}}\right) + 1} \\ &= \frac{\Omega_{c,actual}^2}{s^2 + 1.414\Omega_{c,actual}s + \Omega_{c,actual}^2} \\ &= \frac{0.4251^2}{s^2 + 1.414 \times 0.4251s + 0.4251^2} \\ &= \frac{0.181}{s^2 + 0.601s + 0.181} \end{aligned}$$

- **Step 7: Find the equivalent IIR filter using Bilinear Transform**

Substitute $s \rightarrow \frac{1-z^{-1}}{1+z^{-1}}$.

$$\begin{aligned}
 H(z) &= \frac{0.181}{\left(\frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 0.601\left(\frac{1-z^{-1}}{1+z^{-1}}\right) + 0.181} \\
 &= \frac{0.181(1+2z^{-1}+z^{-2})}{1.782 - 1.638z^{-1} + 0.58z^{-2}} \\
 H(z) &= \frac{0.102 + 0.204z^{-1} + 0.102z^{-2}}{1 - 0.919z^{-1} + 0.325z^{-2}}
 \end{aligned}$$

Final Digital Low pass IIR filter is:

$$H(z) = \frac{0.102 + 0.204z^{-1} + 0.102z^{-2}}{1 - 0.919z^{-1} + 0.325z^{-2}} \quad (15)$$

MATLAB Code

Following is the code snippet. The frequency response and the pole zero plot is as shown in Fig. 3 and 4.

```

1  clc;clear;close all;
2  %% Pass band and Stop Band edges
3  wp = 0.2;
4  ws = 0.5;
5
6  %% Pass band and Stop Band attenuation
7  Ap = 2;
8  As = 15;
9
10 %% Get Cutoff and Order
11 [N wc] = buttord(wp,ws,Ap,As);
12 disp(['Order:' num2str(N)]);
13 disp(['Cutoff: ' num2str(wc)]);
14
15 %% Value of Cutoff in Analog equivalent
16 WW = tan(wc.*pi/2);
17 disp(['Cutoff in Analog: ' num2str(WW)]);
18
19 %% Get Filter Coefficients
20 [b a] = butter(N,wc)
21 %% Get Pole-Zero Plot
22 figure;
23 zplane(b,a);
24 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)
25
26 %% Get Frequency Response
27 figure;
28 freqz(b,a);
29 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)

```

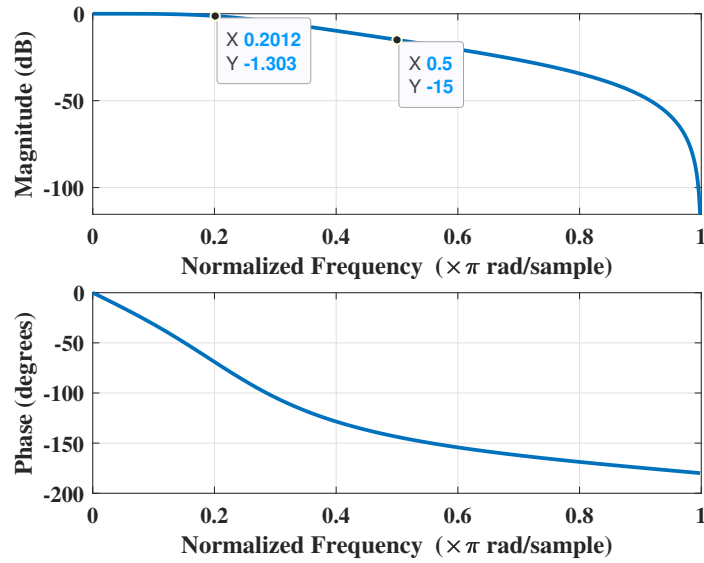


Figure 3: Frequency response for LPF

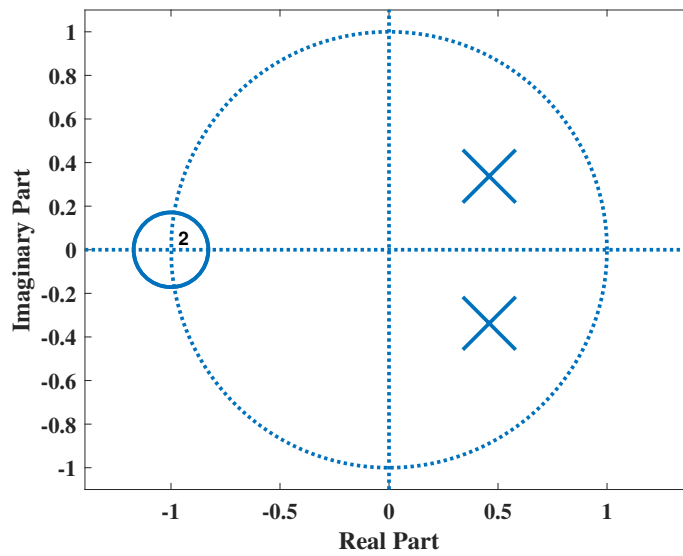


Figure 4: Pole zero for LPF

4 Designing Digital IIR High Pass Filter

Example: Design a high pass filter with following specifications:

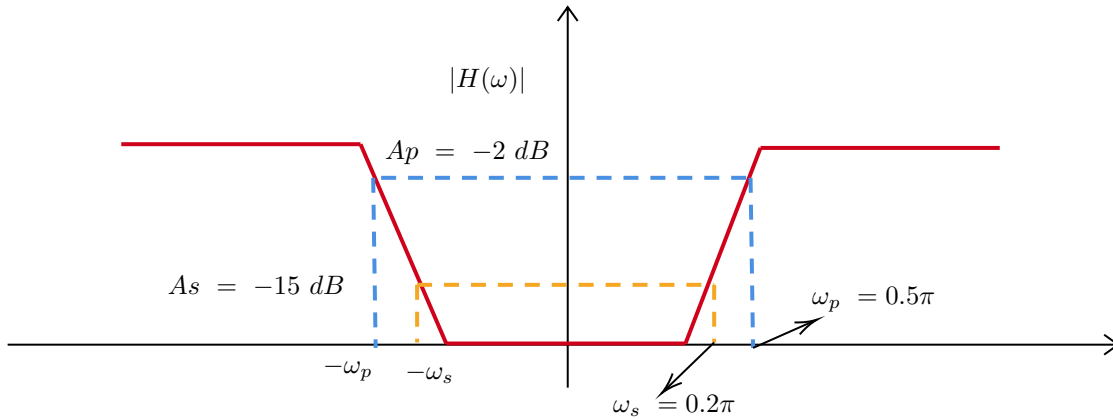


Figure 5: High pass filter specification

- **Step 0: Interpreting the specifications and prewarping the frequencies.**

Following specifications can be observed:

Passband edge: $\omega_p = 0.5\pi$.

Stopband edge: $\omega_s = 0.2\pi$.

Passband attenuation: $A_p = -2dB$.

Stopband attenuation: $A_s = -15dB$.

Prewarping of frequencies:

$$\Omega_{p,HP} = \tan\left(\frac{\omega_p}{2}\right) = \tan\left(\frac{0.5\pi}{2}\right) = 1$$

$$\Omega_{s,HP} = \tan\left(\frac{\omega_s}{2}\right) = \tan\left(\frac{0.2\pi}{2}\right) = 0.3249$$

- **Step 1: Frequency Mapping for Obtaining Normalized LPF**

Butterworth approximation is for Lowpass filter only. If a high pass filter is to be constructed, then it should be mapped to the low pass filter. A typical mapping for a high pass filter is done as,

$$s \rightarrow \frac{1}{s} \quad (16)$$

In frequency terms, it is obtained as,

$$\Omega_{LP} = -\frac{1}{\Omega_{HP}} \quad (17)$$

It is a typical practice that the pass band edge of the lowpass filter is mapped to 1. For that, the RHS of above equation is scaled by Ω_p of the highpass. So, we have,

$$\Omega_{LP} = -\frac{\Omega_{p,HP}}{\Omega_{HP}} \quad (18)$$

The frequency mapping is as shown in Fig. 6.

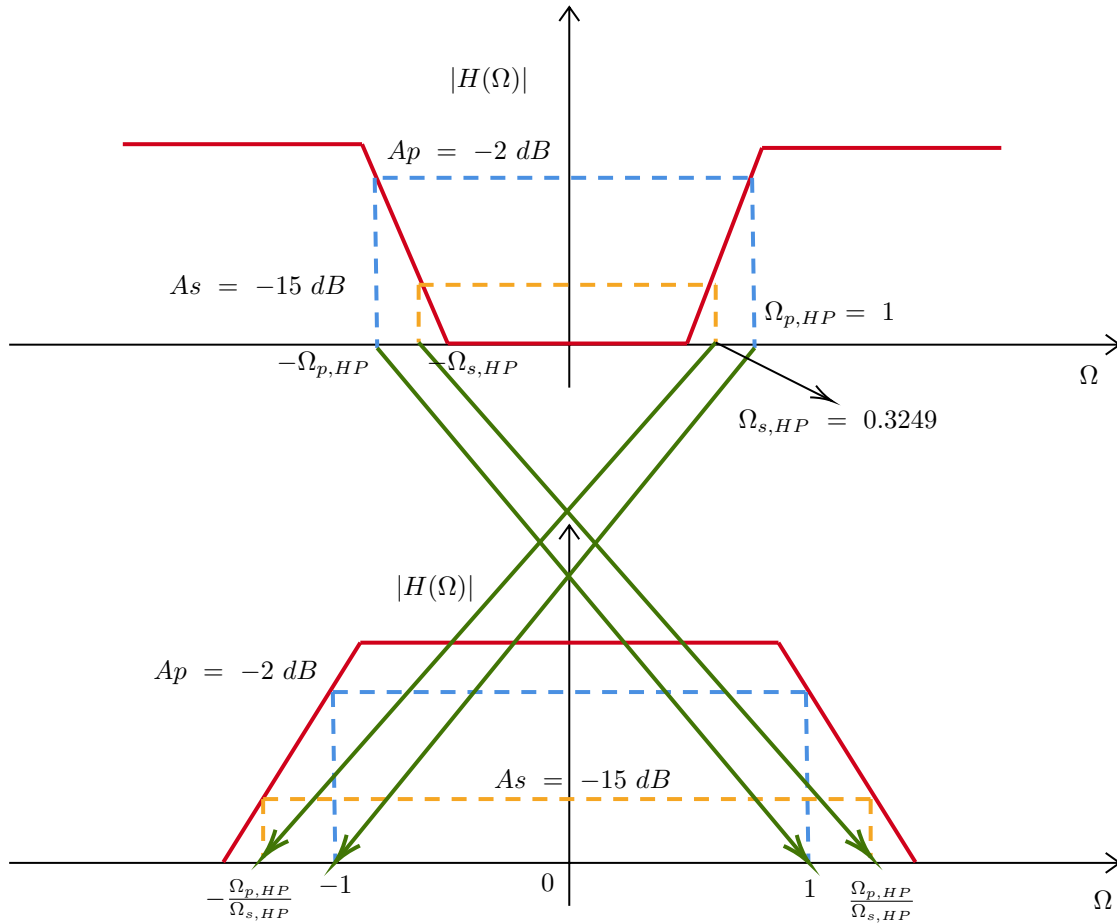


Figure 6: Frequency mapping for HPF

It can be observed that $-\Omega_p$ is mapped to 1 of LPF and $-\Omega_s$ is mapped to $\frac{\Omega_p}{\Omega_s}$. Therefore, the mapped passband and stop band edge of the LPF with passband assumed at 1 is

$$\begin{aligned}\Omega_p &= 1 \\ \Omega_s &= \frac{\Omega_{p,HP}}{\Omega_{s,HP}} = \frac{1}{0.3249} = 3.078\end{aligned}$$

- **Step 2: Finding Order for the Prototype LPF**

The order can be found using the formula

$$N = \frac{\log\left(\frac{10^{|A_s|/10} - 1}{10^{|A_p|/10} - 1}\right)}{2 \times \log\left(\frac{\Omega_s}{\Omega_p}\right)}$$

For considered example,

$$N = \frac{\log\left(\frac{10^{15/10} - 1}{10^{2/10} - 1}\right)}{2 \times \log\left(\frac{0.3249}{1}\right)} = [1.76] = 2.$$

- **Step 3: Find Normalized LPF Equation by Finding roots or Using Polynomial Table**

We have,

$$s_k = e^{j\frac{\pi}{4}(2k+3)} \quad (19)$$

As $N = 2$, $k = \{0, 1\}$. So, we have,

$$s_0 = e^{j\frac{3\pi}{4}}$$

and

$$s_1 = e^{j\frac{5\pi}{4}}$$

Using the roots, the value of $H(s)$ can be found as,

$$\begin{aligned} H(s) &= \frac{1}{(s - s_0)(s - s_1)} \\ &= \frac{1}{(s - e^{j\frac{3\pi}{4}})(s - e^{j\frac{5\pi}{4}})} \\ H(s) &= \frac{1}{s^2 + 1.414s + 1} \end{aligned}$$

- **Step 4: Find the cutoff frequency.**

It can be seen that, the mapped prototype LPF cannot have the cutoff frequency = 1. Hence, there is a need to obtain the required cutoff frequency of the LPF using the formula,

$$\Omega_c = \frac{\Omega_s}{(10^{|A_s|/10} - 1)^{\frac{1}{2N}}} \quad (20)$$

For, this example,

$$\Omega_c = \frac{3.078}{(10^{15/10} - 1)^{\frac{1}{4}}} = 1.3085 \quad (21)$$

- **Step 5: Find Denormalized Cutoff Frequency**

This cutoff frequency is for the LPF mapped with passband edge to 1. The actual cutoff frequency can be calculated as,

$$\Omega_{c,actual} = \frac{\Omega_{p,HP}}{\Omega_c} = \frac{1}{3.078} = 0.764 \quad (22)$$

- **Step 6: Find the Analog Filter**

For mapping the LPF to HPF we need to substitute,

$$s \rightarrow \frac{\Omega_{c,actual}}{s} \quad (23)$$

to get the required HPF. Therefore, the HPF obtained is as shown below.

$$\begin{aligned} H(s) &= \frac{1}{\frac{\Omega_{c,actual}^2}{s^2} + 1.414\frac{\Omega_{c,actual}}{s} + 1} \\ &= \frac{s^2}{s^2 + 1.414\Omega_{c,actual}s + \Omega_{c,actual}^2} \\ &= \frac{s^2}{s^2 + 1.081s + 0.584} \end{aligned}$$

• **Step 7: Find the equivalent IIR filter using Bilinear Transform.**

We have $s \rightarrow \frac{1-z^{-1}}{1+z^{-1}}$. Therefore,

$$\begin{aligned} H(z) &= \frac{\left(\frac{1-z^{-1}}{1+z^{-1}}\right)^2}{\left(\frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 1.081\left(\frac{1-z^{-1}}{1+z^{-1}}\right) + 0.584} \\ &= \frac{1 - 2z^{-1} + z^{-2}}{2.6657 - 0.831z^{-1} + 0.5035z^{-2}} \\ &= \frac{0.375 - 0.751z^{-1} + 0.375z^{-2}}{1 - 0.3126z^{-1} + 0.1891z^{-2}} \end{aligned}$$

The final High pass filter is obtained as,

$$H(z) = \frac{0.375 - 0.751z^{-1} + 0.375z^{-2}}{1 - 0.3126z^{-1} + 0.1891z^{-2}} \quad (24)$$

MATLAB Code

Following is the code snippet. The frequency response and the pole zero plots are as shown in Fig. 7 and 8 respectively.

```

1  clc;clear;close all;
2  %% Pass band and Stop Band edges
3  wp = 0.5;
4  ws = 0.2;
5
6  %% Pass band and Stop Band attenuation
7  Ap = 2;
8  As = 15;
9
10 %% Get Cutoff and Order
11 [N wc] = buttord(wp,ws,Ap,As);
12 disp(['Order:' num2str(N)]);
13 disp(['Cutoff: ' num2str(wc)]);
14
15 %% Value of Cutoff in Analog equivalent
16 WW = tan(wc.*pi/2);
17 disp(['Cutoff in Analog: ' num2str(WW)]);
18
19 %% Get Filter Coefficients
20 [b a] = butter(N,wc,'high')
21 %% Get Pole-Zero Plot
22 figure;
23 zplane(b,a);
24 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)
25
26 %% Get Frequency Response
27 figure;
28 freqz(b,a);
29 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)

```

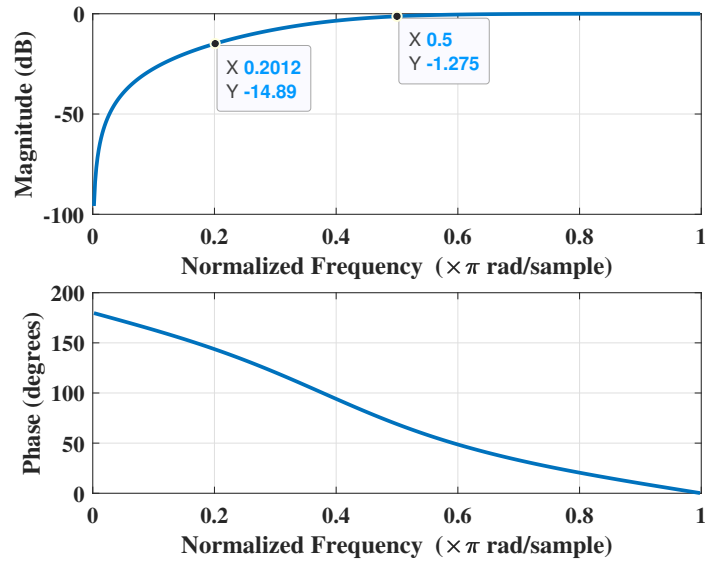


Figure 7: Frequency response for HPF

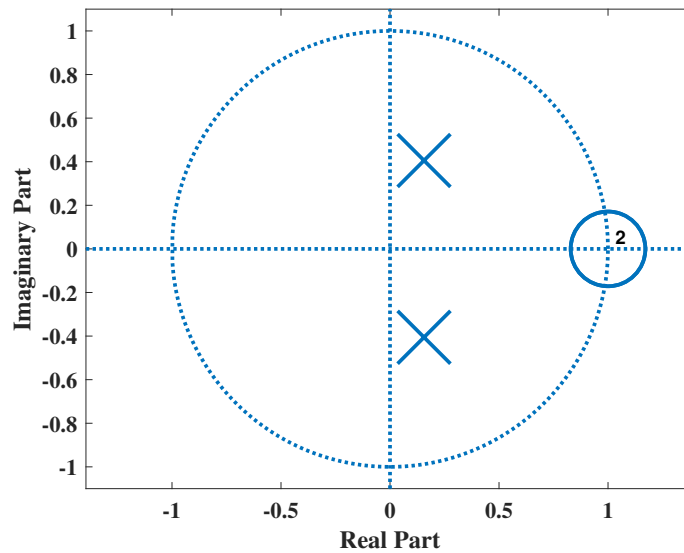


Figure 8: Pole zero for HPF

5 Designing Digital IIR Band Pass Filter

Example: Design the Digital IIR Bandpass filter with following specifications:

1. Lower stop band edge: 0.1π

2. Lower pass band edge: 0.4π
3. Higher pass band edge: 0.6π
4. Higher stop band edge: 0.9π
5. Pass band attenuation: -3 dB
6. Stop band attenuation: -18 dB

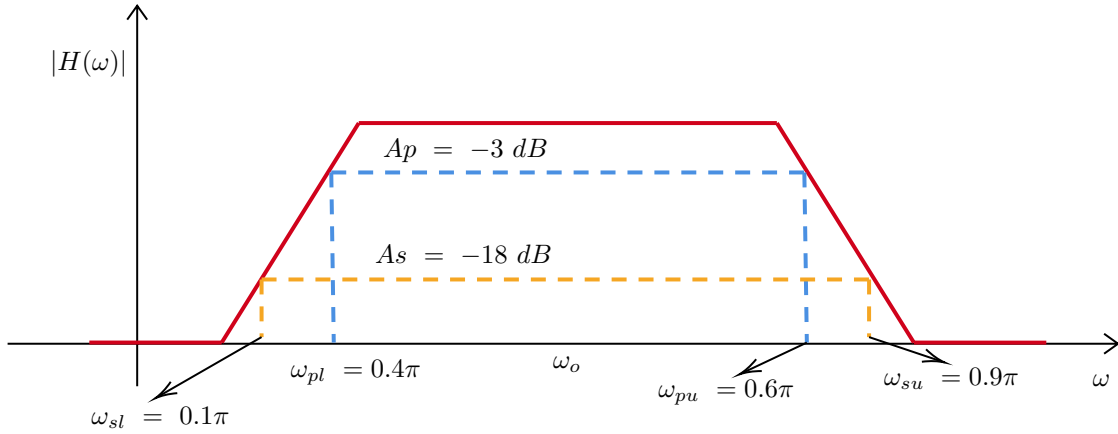


Figure 9: Band Pass Filter Specification

- **Step 0: Interpreting the specifications and prewarping the frequencies**

$$\Omega_{sl} = \tan\left(\frac{\omega_{sl}}{2}\right) = \tan\left(\frac{0.1\pi}{2}\right) = \tan(0.05\pi) = 0.15838$$

$$\Omega_{pl} = \tan\left(\frac{\omega_{pl}}{2}\right) = \tan\left(\frac{0.4\pi}{2}\right) = \tan(0.2\pi) = 0.72654$$

$$\Omega_{pu} = \tan\left(\frac{\omega_{pu}}{2}\right) = \tan\left(\frac{0.6\pi}{2}\right) = \tan(0.3\pi) = 1.37638$$

$$\Omega_{su} = \tan\left(\frac{\omega_{su}}{2}\right) = \tan\left(\frac{0.9\pi}{2}\right) = \tan(0.45\pi) = 6.31375$$

- **Step 1: Frequency Mapping for Obtaining Normalized LPF**

The bandpass filter is to be mapped to low pass filter in order to use Butterworth approximation. The mapping used is:

$$s \rightarrow \frac{s^2 + \Omega_o^2}{Bs} \quad (25)$$

where, $B = \Omega_{pu} - \Omega_{pl}$ and Ω_o is the center frequency which is geometric mean of any two frequencies on its either side that correspond to same magnitude. In general, the passband frequencies are considered. Therefore, $\Omega_o^2 = \Omega_{pu} \times \Omega_{pl}$. The mapping reduces to,

$$s \rightarrow \frac{s^2 + \Omega_{pu} \times \Omega_{pl}}{s(\Omega_{pu} - \Omega_{pl})} \quad (26)$$

and the frequency mappings are given as,

$$\Omega_{LP} \rightarrow \frac{\Omega_{BP}^2 - \Omega_{pu} \times \Omega_{pl}}{\Omega_{BP}(\Omega_{pu} - \Omega_{pl})} \quad (27)$$

where, Ω_{BP} and Ω_{LP} are the frequencies corresponding to BPF and prototype LPF respectively. We have,

$$B = \Omega_{pu} - \Omega_{pl} = 0.64984$$

$$\Omega_o^2 = \Omega_{pu} \times \Omega_{pl} = 1$$

The pass band and stop band edges when mapped lead to,

$$\Omega_{sl} = 0.15838 \rightarrow \frac{0.15838^2 - 1}{0.15838 \times 0.64984} = -9.4721$$

$$\Omega_{pl} = 0.72654 \rightarrow \frac{0.72654^2 - 1}{0.72654 \times 0.64984} = -1$$

$$\Omega_{pu} = 1.37638 \rightarrow \frac{1.37638^2 - 1}{1.37638 \times 0.64984} = 1$$

$$\Omega_{su} = 6.31375 \rightarrow \frac{6.31375^2 - 1}{6.31375 \times 0.64984} = 9.4721$$

$$\Omega_0 = 1 \rightarrow \frac{1 - 1}{1 \times 0.64984} = 0$$

The mapping can be easily visualized graphically as shown in Fig. 10.

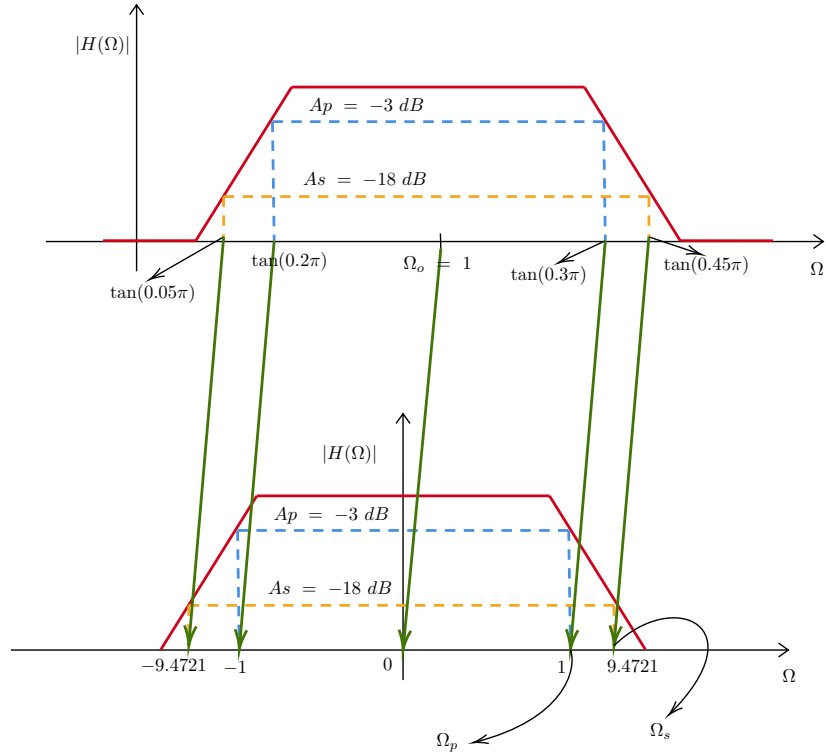


Figure 10: Mapping for Bandpass Filter

Therefore, the mapped frequencies for LPF can be obtained as,

$$\Omega_p = 1$$

$$\Omega_s = \frac{\Omega_{su}^2 - \Omega_{pu} \times \Omega_{pl}}{\Omega_{su}(\Omega_{pu} - \Omega_{pl})} = 9.4721$$

- **Step 2: Finding Order for the Prototype LPF**

The order can be found as,

$$N = \frac{\log\left(\frac{10^{|A_s|/10} - 1}{10^{|A_p|/10} - 1}\right)}{2 \times \log\left(\frac{\Omega_s}{\Omega_p}\right)}$$

For considered example,

$$N = \frac{\log\left(\frac{10^{18/10} - 1}{10^{3/10} - 1}\right)}{2 \times \log\left(\frac{9.4721}{1}\right)} = [0.9192] = 1.$$

- **Step 3: Find Normalized LPF Equation by Finding roots or Using Polynomial Table**

From Table 1, we have

$$H(s) = \frac{1}{s + 1} \quad (28)$$

- **Step 4: Find the cutoff frequency.**

The cutoff frequency can be calculated as,

$$\Omega_c = \frac{\Omega_s}{(10^{|A_s|/10} - 1)^{\frac{1}{2N}}} \quad (29)$$

For this example,

$$\Omega_c = \frac{9.4721}{(10^{18/10} - 1)^{\frac{1}{2}}} = 1.202 \quad (30)$$

- **Step 5: Find Denormalized Cutoff Frequency**

The cutoff frequencies for the BPF can be found as,

$$\begin{aligned} \Omega_{c1} &= -\frac{\Omega_c B}{2} + \frac{1}{2} \sqrt{\Omega_c^2 B^2 + 4\Omega_o^2} \\ &= -\frac{1.202 \times 0.64984}{2} + \frac{1}{2} \sqrt{1.202^2 \times 0.64984^2 + 4 \times 1} = 0.6830 \\ \Omega_{c2} &= +\frac{\Omega_c B}{2} + \frac{1}{2} \sqrt{\Omega_c^2 B^2 + 4\Omega_o^2} \\ &= \frac{1.202 \times 0.64984}{2} + \frac{1}{2} \sqrt{1.202^2 \times 0.64984^2 + 4 \times 1} = 1.4641 \end{aligned}$$

- **Step 6: Find the Analog Filter**

In order to obtain the bandpass filter from lowpass filter, we substitute,

$$s \rightarrow \frac{s^2 + \Omega_o^2}{(\Omega_{c2} - \Omega_{c1})s} \quad (31)$$

Therefore, the Bandpass filter obtained after transformation,

$$\begin{aligned} H(s) &= \frac{1}{\frac{s^2+1}{(1.4641-0.6830)s} + 1} \\ &= \frac{1}{\frac{s^2+1}{0.7811s} + 1} \\ H(s) &= \frac{0.7811s}{s^2 + 0.7811s + 1} \end{aligned}$$

• **Step 7: Find the equivalent IIR filter using Bilinear Transform.**

Bilinear transformation is given as $s \rightarrow \frac{1-z^{-1}}{1+z^{-1}}$. Therefore,

$$\begin{aligned} H(z) &= \frac{0.7811 \left(\frac{1-z^{-1}}{1+z^{-1}} \right)}{\left(\frac{1-z^{-1}}{1+z^{-1}} \right)^2 + 0.7811 \left(\frac{1-z^{-1}}{1+z^{-1}} \right) + 1} \\ H(z) &= \frac{0.2809 - 0.2809z^{-2}}{1 + 0.4383z^{-2}} \end{aligned}$$

The final bandpass filter is obtained as,

$$H(z) = \frac{0.2809 - 0.2809z^{-2}}{1 + 0.4383z^{-2}} \quad (32)$$

MATLAB Code

Following is the code snippet for Bandpass filter. The frequency response and the pole zero plot is as shown in Fig. 11 and 12 respectively.

```

1  clc;clear;close all;
2  %% Pass band and Stop Band edges
3  wp = [0.4 0.6];
4  ws = [0.1 0.9];
5
6  %% Pass band and Stop Band attenuation
7  Ap = 3;
8  As = 18;
9
10 %% Get Cutoff and Order
11 [N wc] = buttord(wp,ws,Ap,As);
12 disp(['Order: ' num2str(N)]);
13 disp(['Cutoff: ' num2str(wc)]);
14
15 %% Value of Cutoff in Analog equivalent
16 WW = tan(wc.*pi/2);
17 disp(['Cutoff in Analog: ' num2str(WW)]);
18
19 %% Get Filter Coefficients

```



```
20 [b a] = butter(N,wc,'bandpass')
21 %% Get Pole-Zero Plot
22 figure;
23 zplane(b,a);
24 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)
25
26 %% Get Frequency Response
27 figure;
28 freqz(b,a);
29 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)
```

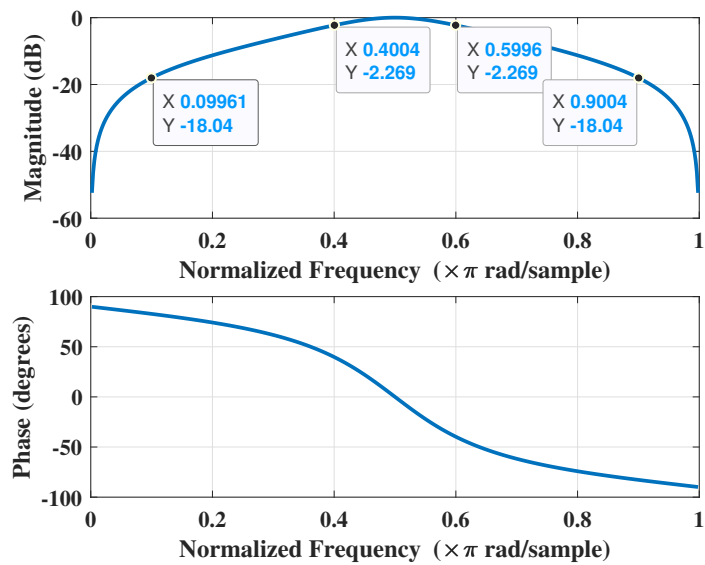


Figure 11: Frequency response for BPF

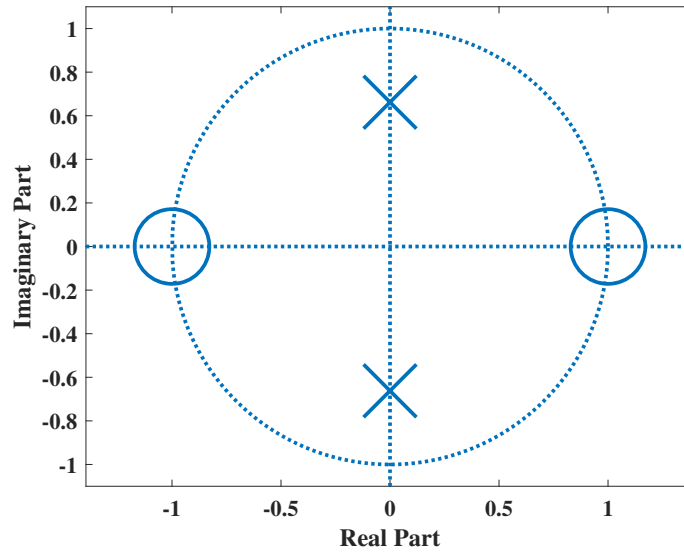


Figure 12: Pole zero for BPF

6 Designing Digital IIR Band Stop Filter

Example: Design a Digital IIR Band stop filter with following specifications.

1. Lower pass band edge: 0.1π
2. Lower stop band edge: 0.4π
3. Higher stop band edge: 0.6π
4. Higher pass band edge: 0.9π
5. Pass band attenuation: -3 dB
6. Stop band attenuation: -18 dB

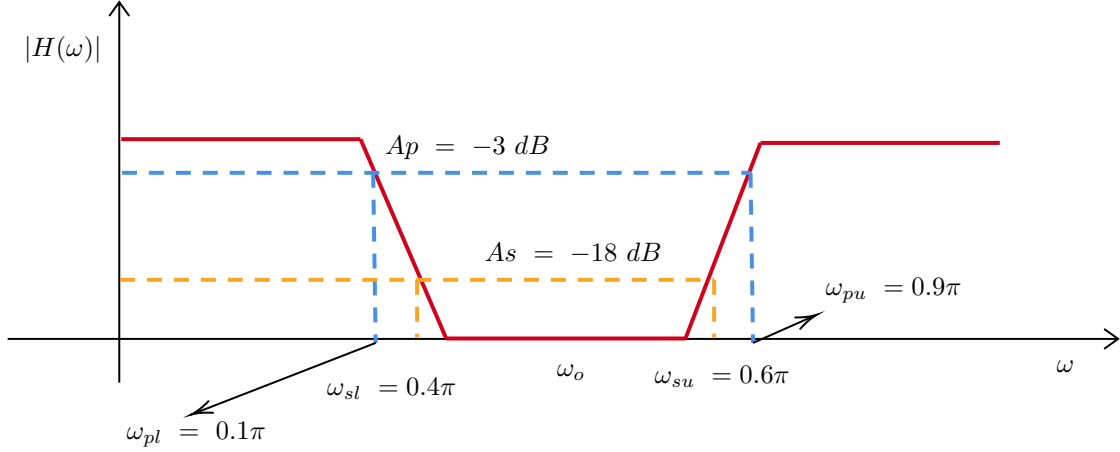


Figure 13: Band Stop Filter Specifications

- **Step 0: Interpreting the specifications and prewarping the frequencies**

$$\Omega_{pl} = \tan\left(\frac{\omega_{pl}}{2}\right) = \tan\left(\frac{0.1\pi}{2}\right) = \tan(0.05\pi) = 0.15838$$

$$\Omega_{sl} = \tan\left(\frac{\omega_{sl}}{2}\right) = \tan\left(\frac{0.4\pi}{2}\right) = \tan(0.2\pi) = 0.72654$$

$$\Omega_{su} = \tan\left(\frac{\omega_{su}}{2}\right) = \tan\left(\frac{0.6\pi}{2}\right) = \tan(0.3\pi) = 1.37638$$

$$\Omega_{pu} = \tan\left(\frac{\omega_{pu}}{2}\right) = \tan\left(\frac{0.9\pi}{2}\right) = \tan(0.45\pi) = 6.31375$$

- **Step 1: Frequency Mapping for Obtaining Normalized LPF**

The band stop filter is to be mapped to low pass filter in order to use Butterworth approximation. The mapping used is:

$$s \rightarrow \frac{Bs}{s^2 + \Omega_o^2} \quad (33)$$

where, $B = \Omega_{pu} - \Omega_{pl}$ and Ω_o is the center frequency which is geometric mean of any two frequencies on its either side that correspond to same magnitude. In general, the passband frequencies are considered. Therefore, $\Omega_o^2 = \Omega_{pu} \times \Omega_{pl}$. The mapping reduces to,

$$s \rightarrow \frac{s(\Omega_{pu} - \Omega_{pl})}{s^2 + \Omega_{pu} \times \Omega_{pl}} \quad (34)$$

and the frequency mappings are given as,

$$\Omega_{LFP} \rightarrow \frac{\Omega_{BS}(\Omega_{pu} - \Omega_{pl})}{\Omega_{pu} \times \Omega_{pl} - \Omega_{BS}^2} \quad (35)$$

where, Ω_{BS} and Ω_{LFP} are the frequencies corresponding to BSF and prototype LPF respectively. Here,

$$B = \Omega_{pu} - \Omega_{pl} = 6.15537$$

$$\Omega_o^2 = \Omega_{pu} \times \Omega_{pl} = 1$$

The pass band and stop band edges when mapped lead to,

$$\Omega_{pl} = 0.15838 \rightarrow \frac{6.15537 \times 0.15838}{1 - 0.15838^2} = 1$$

$$\Omega_{sl} = 0.72654 \rightarrow \frac{6.15537 \times 0.72654}{1 - 0.72654^2} = 9.4721$$

$$\Omega_{su} = 1.37638 \rightarrow \frac{6.15537 \times 1.37638}{1 - 1.37638^2} = -9.4721$$

$$\Omega_{pu} = 6.31375 \rightarrow \frac{6.15537 \times 6.31375}{1 - 6.31375^2} = -1$$

$$\Omega_o = 1 \rightarrow \frac{6.15537 \times 1}{1 - 1^2} = \infty$$

The mapping for the BSF is as shown in Fig. 14.

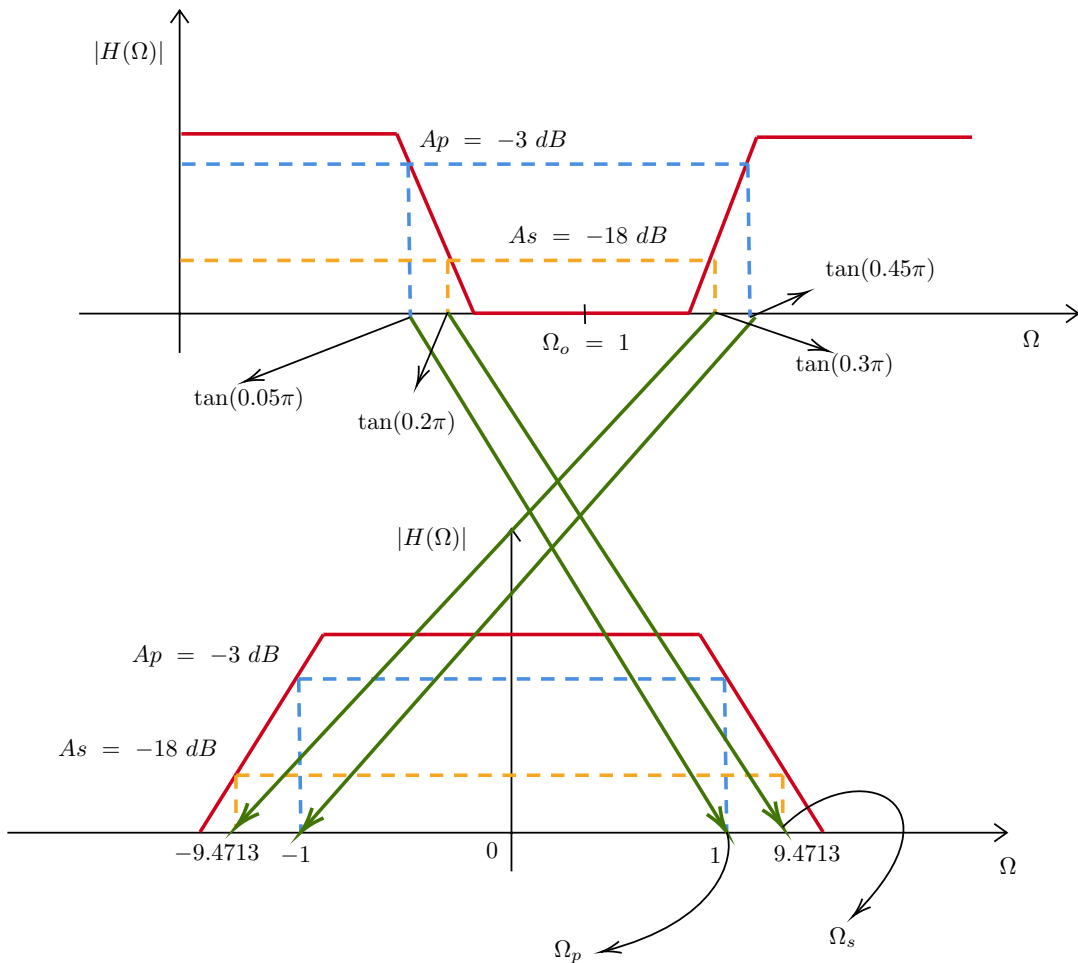


Figure 14: Frequency Mapping for Band Stop Filter

Therefore, the mapped frequencies for LPF can be obtained as,

$$\begin{aligned}\Omega_p &= 1 \\ \Omega_s &= \frac{\Omega_{sl}(\Omega_{pu} - \Omega_{pl})}{\Omega_{pu} \times \Omega_{pl} - \Omega_{sl}^2} = 9.4721\end{aligned}$$

- **Step 2: Finding Order for the prototype LPF**

The order can be found as,

$$N = \frac{\log\left(\frac{10^{|A_s|/10} - 1}{10^{|A_p|/10} - 1}\right)}{2 \times \log\left(\frac{\Omega_s}{\Omega_p}\right)}$$

For considered example,

$$N = \frac{\log\left(\frac{10^{18/10} - 1}{10^{3/10} - 1}\right)}{2 \times \log\left(\frac{9.4721}{1}\right)} = [0.9192] = 1.$$

- **Step 3: Find Normalized LPF Equation by Finding roots or Using Polynomial Table.**

From Table 1, the normalized LPF is given as,

$$H(s) = \frac{1}{s + 1} \quad (36)$$

- **Step 4: Find the cutoff frequency**

The cutoff frequency can be calculated as,

$$\Omega_c = \frac{\Omega_s}{(10^{|A_s|/10} - 1)^{\frac{1}{2N}}} \quad (37)$$

For this example,

$$\Omega_c = \frac{9.4721}{(10^{18/10} - 1)^{\frac{1}{2}}} = 1.202 \quad (38)$$

- **Step 5: Find Denormalized Cutoff Frequency**

The cutoff frequency for the BSF can be found as,

$$\begin{aligned}\Omega_{c1} &= -\frac{B}{2\Omega_c} + \frac{1}{2}\sqrt{\frac{B^2}{\Omega_c^2} + 4\Omega_o^2} \\ &= -\frac{6.15537}{2 \times 1.202} + \frac{1}{2}\sqrt{\frac{6.15537^2}{1.202^2} + 4 \times 1} = 0.1883 \\ \Omega_{c2} &= +\frac{B}{2\Omega_c} + \frac{1}{2}\sqrt{\frac{B^2}{\Omega_c^2} + 4\Omega_o^2} \\ &= -\frac{6.15537}{2 \times 1.202} + \frac{1}{2}\sqrt{\frac{6.15537^2}{1.202^2} + 4 \times 1} = 5.3093\end{aligned}$$

- **Step 6: Find the Analog Filter**

In order to obtain the bandstop filter from lowpass filter, we substitute,

$$s \rightarrow \frac{(\Omega_{c2} - \Omega_{c1})s}{s^2 + 1} \quad (39)$$

Therefore, the Bandstop filter obtained after transformation,

$$\begin{aligned} H(s) &= \frac{1}{\frac{(5.3093-0.1883)s}{s^2+1} + 1} \\ &= \frac{1}{\frac{5.121s}{s^2+1} + 1} \\ H(s) &= \frac{s^2 + 1}{s^2 + 5.121s + 1} \end{aligned}$$

- **Step 7: Find the equivalent IIR filter using Bilinear Transform**

Bilinear transformation is given as $s \rightarrow \frac{1-z^{-1}}{1+z^{-1}}$. Therefore,

$$\begin{aligned} H(z) &= \frac{\left(\frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 1}{\left(\frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 5.121\left(\frac{1-z^{-1}}{1+z^{-1}}\right) + 1} \\ &= \frac{2 + 2z^{-2}}{7.1209 - 3.121z^{-2}} \\ H(z) &= \frac{0.2809 + 0.2809z^{-2}}{1 - 0.4383z^{-2}} \end{aligned}$$

The final bandstop filter is obtained as,

$$H(z) = \frac{0.2809 + 0.2809z^{-2}}{1 - 0.4383z^{-2}} \quad (40)$$

MATLAB Code

Following is the code snippet. The frequency response and the pole zero plot is as shown in Fig. 15 and 16 respectively.

```

1  clc;clear;close all;
2  %% Pass band and Stop Band edges
3  ws = [0.4 0.6];
4  wp = [0.1 0.9];
5
6  %% Pass band and Stop Band attenuation
7  Ap = 3;
8  As = 18;
9
10 %% Get Cutoff and Order
11 [N wc] = buttord(wp,ws,Ap,As);
12 disp(['Order:' num2str(N)]);
13 disp(['Cutoff: ' num2str(wc)]);
14

```

```

15 %% Value of Cutoff in Analog equivalent
16 WW = tan(wc.*pi/2);
17 disp(['Cutoff in Analog: ' num2str(WW)]);
18
19 %% Get Filter Coefficients
20 [b a] = butter(N,wc,'stop')
21 %% Get Pole-Zero Plot
22 figure;
23 zplane(b,a);
24 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)
25
26 %% Get Frequency Response
27 figure;
28 freqz(b,a);
29 set(findall(gcf,'Type','line'),'LineWidth',2,'MarkerSize',40)

```

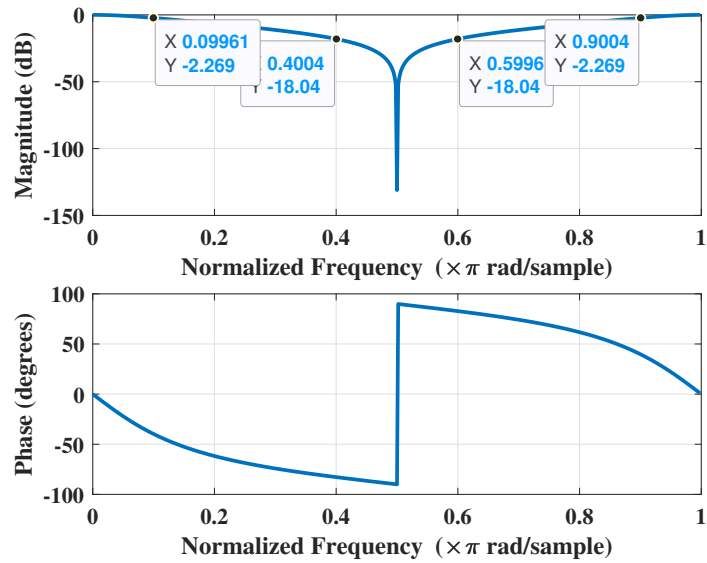


Figure 15: Frequency response for BSF

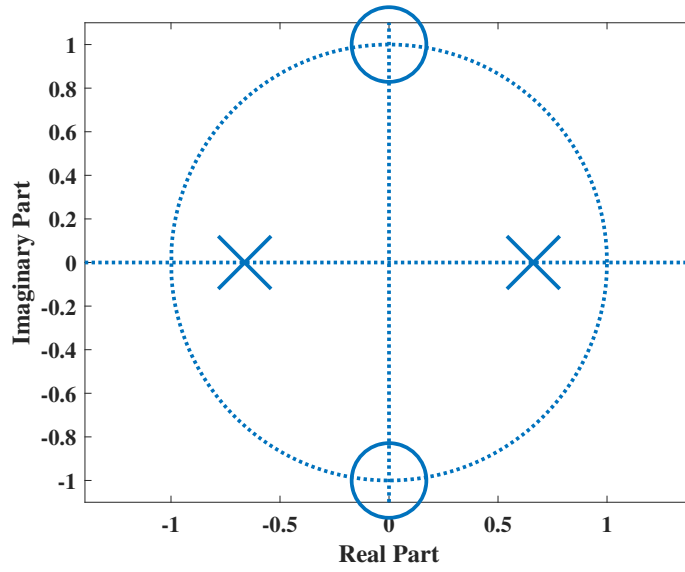


Figure 16: Pole zero for SBF

7 Summary:

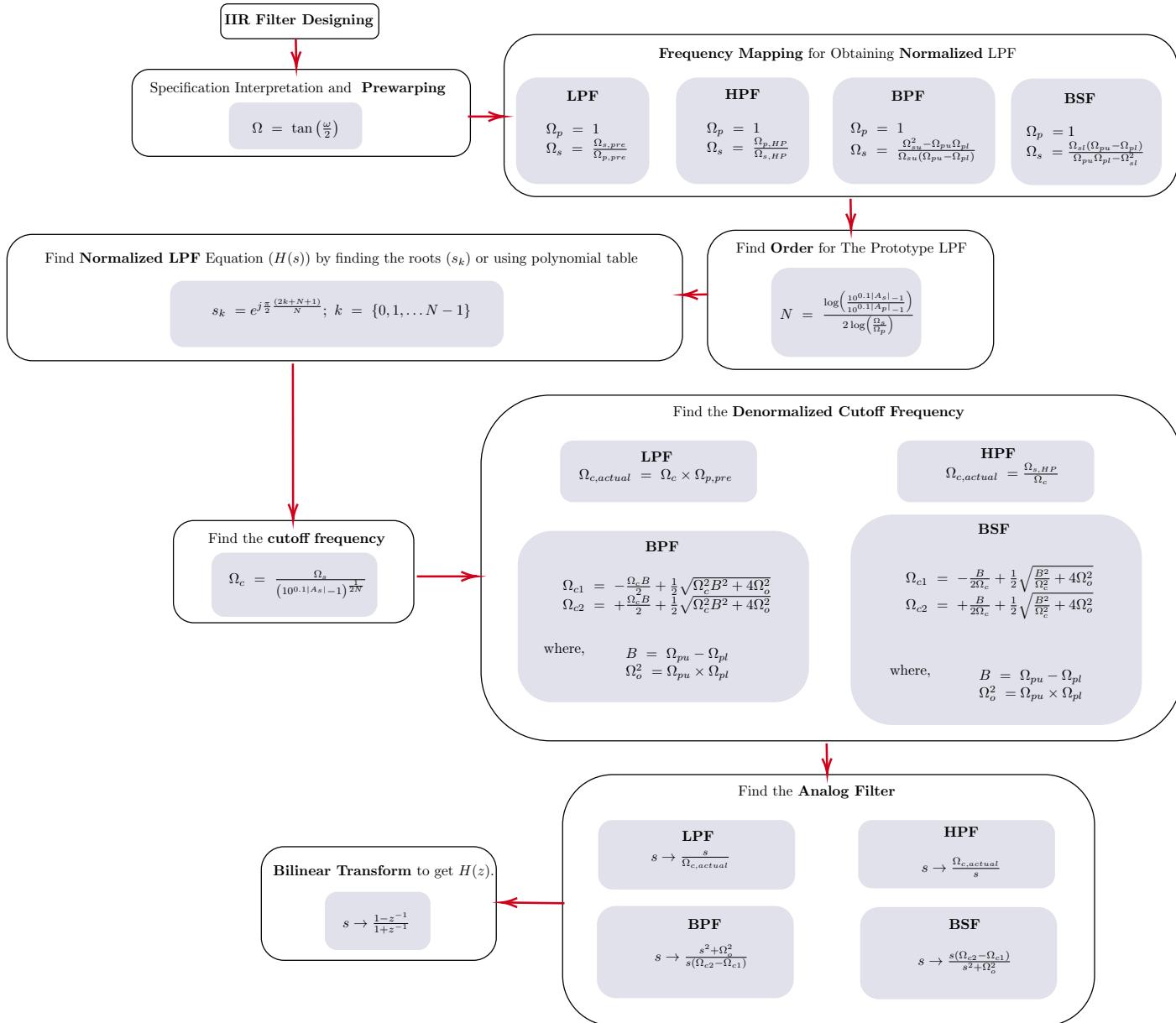


Figure 17: Summary of the IIR Filter Design

Table 2: Typical Frequency Mappings

Frequencies	Frequencies Mapped for prototype LPF			
	LPF	HPF	BPF	BSF
Ω	$\frac{\Omega}{\Omega_{p,LP}}$	$-\frac{\Omega_{p,HP}}{\Omega}$	$\frac{\Omega^2 - \Omega_{pu} \times \Omega_{pl}}{\Omega(\Omega_{pu} - \Omega_{pl})}$	$\frac{\Omega(\Omega_{pu} - \Omega_{pl})}{\Omega_{pu} \times \Omega_{pl} - \Omega^2}$
$-\infty$	$-\infty$	0	$-\infty$	0
0	0	∞	∞	0
∞	∞	0	∞	0
Center Frequency (Ω_o) (For BPF and BSF)	-	-	0	∞
$-\Omega_p$	-1	1	-	-
Ω_p	1	-1	-	-
$-\Omega_s$	$-\frac{\Omega_s}{\Omega_{p,LP}}$	$\frac{\Omega_{p,HP}}{\Omega_s}$	-	-
Ω_s	$\frac{\Omega_s}{\Omega_{p,LP}}$	$\frac{\Omega_{p,HP}}{\Omega}$	-	-
Ω_{pl}	-	-	-1	1
Ω_{pu}	-	-	1	-1
Ω_{sl}	-	-	$\frac{\Omega_{sl}^2 - \Omega_{pu} \times \Omega_{pl}}{\Omega_{sl}(\Omega_{pu} - \Omega_{pl})} = -\frac{\Omega_{su}^2 - \Omega_{pu} \times \Omega_{pl}}{\Omega_{su}(\Omega_{pu} - \Omega_{pl})}$	$\frac{\Omega_{sl}(\Omega_{pu} - \Omega_{pl})}{\Omega_{pu} \times \Omega_{pl} - \Omega_{sl}^2}$
Ω_{su}	-	-	$\frac{\Omega_{su}^2 - \Omega_{pu} \times \Omega_{pl}}{\Omega_{su}(\Omega_{pu} - \Omega_{pl})}$	$\frac{\Omega_{su}(\Omega_{pu} - \Omega_{pl})}{\Omega_{pu} \times \Omega_{pl} - \Omega_{su}^2} = -\frac{\Omega_{sl}(\Omega_{pu} - \Omega_{pl})}{\Omega_{pu} \times \Omega_{pl} - \Omega_{sl}^2}$